



# Cell-Free Layer (CFL) Analysis in a Polydimethylsiloxane (PDMS) Microchannel: a Global Approach

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# Cell-Free Layer (CFL) Analysis in a Polydimethylsiloxane (PDMS) Microchannel: a Global Approach

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## Abstract

The cell-free layer (CFL) is a hemodynamic phenomenon that has an important contribution to the rheological properties of blood flowing in microvessels. The present work aims to find the closest function describing RBCs flowing around the cell depleted layer in a polydimethylsiloxane (PDMS) microchannel with a diverging and a converging bifurcation. The flow behavior of the CFL was investigated by using a high-speed video microscopy system where special attention was devoted to its behavior before the bifurcation and after the confluence of the microchannel. The numerical data was first obtained by using a manual tracking plugin and then analysed by an optimization technique using the genetic algorithm approach. The results show that for the majority of the cases the function that more closely resembles the CFL boundary is the trigonometric function.

## Introduction

Blood is a complex fluid composed mainly of suspended red blood cells (RBCs) within plasma where RBCs are responsible for the supply of oxygen and nutrients to the body and removal of carbon dioxide and metabolic wastes from tissues. Throughout the years, several experimental methods were performed in both in vivo [1-4] and in vitro [5-11] environments, in an attempt to understand the flow behavior of RBCs in microchannels and microvessels. These studies have produced significant findings with respect to rheological properties of RBCs. A hemodynamic phenomenon observed in both in vivo and in vitro studies is the formation of a marginal cell-free layer (CFL) at regions adjacent to wall due to the tendency of RBCs to migrate toward the centre

of the microtube [1, 10, 12]. The existence of a cell depleted layer in microvessels, tend to reduce the apparent viscosity of blood and by increasing this layer the blood viscosity tend to decrease in both microchannels and microvessels. Hence, it is

important to understand the behavior of the CFL in microcirculation as it contributes to the rheological properties of blood flowing in microvessels, modulates the nitric oxide scavenging effects by RBCs and may lead to heterogeneous distribution of blood cells in microvascular networks [4, 13].

Although in vivo and vitro experiments give a more realistic information on the flow properties of blood, once validated, physical models and their numerical results are extremely valuable tools to obtain more insight on the blood rheological properties at a micro-scale level. Recently due to the advances of the computational techniques and computing power, several numerical models have been proposed based on a multiphase approach, in which the blood is considered as a multiphase suspension of deformable particles and where levels of submodeling for the blood cells behaviour are also taken into account. Some examples for this type of approach are the boundary element method [14, 15], the immersed boundary method [16, 17], the lattice Boltzmann method [18, 19] the moving particle semi-implicit (MPS) method [20-23] and spring– network model based on the minimum energy concept [24, 25]. Recent reviews on these numerical methods can be found in Liu et al. [26], Yamaguchi et al. [27] and Lima et al. [10]. Although multiphase approaches are promising methods, it is still extremely complex to consider the CFL in their numerical models. The present study tracks RBCs flowing around the CFL and calculates the most suitable function by using global optimization technique. The measurements were performed in a polydimethylsiloxane (PDMS) microchannel with a diverging and a converging bifurcation and all images were obtained by means of a high-speed video microscopy system.

The paper is organized as follows. First section shows the materials used in this work and the methods that were applied in this study. The second section presents the numerical results and discussion. The last section presents the main conclusions and some future directions.

## Materials and Methods

## Microfabrication

Microchannels were initially developed with a CAD software, where the geometries were selected taking into account a previous study about the blood flowing through microchannels with bifurcations and confluences fabricated by a soft lithography technique [9]. The parent microchannels have 300, 500 and 1000  $\mu\text{m}$  in width and the two branches of the bifurcation and confluence corresponds to 50% of the width of parent channel [28]. Illustration 1 shows the configuration of the network and the regions where the CFL was measured.

This geometry was used to fabricate the molds by using a soft xurography technique [28]. The mold was used for the production of PDMS microchannels. The PDMS was obtained by mixing a curing agent (10:1 ratio) with PDMS prepolymer. By using of a spin coater, a residual amount of PDMS with a ratio 20:1 was dispersed on a slide glass. The PDMS was cured in an oven at 80  $^{\circ}\text{C}$  for 20 minutes. Then by using a blade the microchannels were cutted off and the inlet/outlet holes of the fluid were done by using a fluid dispensing tip. Finally, to have a strong adhesion of the materials, the device was placed in the oven at 80  $^{\circ}\text{C}$  for 24 hours.

## Experimental Set-up

The fabricated microchannels were used to study *in vitro* blood flow with Dextran 40 containing 10% of RBCs. The blood was collected from a healthy sheep and heparin was added to prevent clotting. Additionally, the cells were separated from blood by centrifugation.

A syringe pump (*Harvard Apparatus PHD ULTRA™*) was used to control the flow rate of the working fluid. To visualize and measure the flow we have used an inverted microscope (*IX71, Olympus*) combined with a high speed camera (*i-SPEED LT*). Illustration 2 shows the experimental apparatus used to control the flow and to visualize the CFL within the microchannels. The microfluidic device containing the microchannels was placed on the stage of the inverted microscope and a pressure-driven flow was kept constant by means of a syringe pump. All images have a resolution of 800x600 pixels and were recorded at a frame rate of 200 frames/s.

## Image Analysis

A manual tracking plugin (MTrackJ), of the image analysis software Image J, was used to track individual RBC flowing around the boundary of the RBCs core. By using MTrackJ plugin, the centroid of the selected RBC was automatically computed. After

obtaining  $x$  and  $y$  coordinates of the RBC centroids, the data were exported for the determination of each individual RBC trajectory [5]. Illustration 3 shows a trajectory of a RBC flowing around the boundary region between the CFL and RBCs core.

## Global optimization method: Genetic Algorithm

Genetic algorithms are based on theory of evolution of species from Darwin. This method allows to find a global minimum in a large search space [29]. The genetic algorithm starts with a set of solutions called population, where the solution is represented by an individual and the population size is preserved through each generation. The objective function is evaluated in each individual. Then individuals are selected according to their objective value. Those selected will be reproduced up randomly, by using genetic operators such as mutation and crossover. Individuals with less values have a high probability of being selected whereas the new generation of individuals may have a minor objective value than the previous generation. The evolution process is repeated until the stopping criterion is satisfied [30, 31]. By using this method, RBC trajectories obtained are approximated and most suitable function is found out.

## Results and Discussion

All videos captured were recorded in four different regions, i. e., region 1 and 3 correspond to locations before the bifurcation whereas region 2 and 4 correspond to locations after the confluence (see illustration 1). Moreover, this study was investigated the CFL behaviour in three kinds of parent microchannels having widths of 300, 500 and 1000  $\mu\text{m}$ . For all the cases, the flow rate was constant (10 $\mu\text{l}/\text{min}$ ) and the working fluid had always a haematocrit of 10%, i. e., containing 10% of ovine RBCs in the solution.

A manual tracking plugin from Image J was used to track individual RBC flowing around the boundary region between the CFL and RBCs core. All the selected RBCs have enough good quality images to track the trajectory of the cells flowing nearby the RBCs core (see Illustration 3). Illustration 4 shows representative RBC trajectories in the different cases under study, i. e., parent microchannels with widths of 300, 500 and 1000  $\mu\text{m}$  at two different regions (region before the bifurcation and after the confluence).

To obtain the numerical data a nonlinear least squares theory was used. In each region  $R_{Aw}$ ,  $R_{Bw}$ ,  $R_{Cw}$  and  $R_{Dw}$  for  $w = 300, 500$  and  $1000$ , we have applied the nonlinear optimization problem defined in illustration 5.

After developing a MatLab code and by applying the

genetic algorithm to solve the optimization problem (1), it was possible to obtain the numerical results shown in Table 1. Since the genetic algorithm is a stochastic method, each problem was solved 100 times. Table 1 presents the regions where the problem (1) was applied, the average of the optimum value and the minimum value obtained in the all 100 runs. The table shows that the minimum value for most of the cases corresponds to the function  $g_3$ .

Illustration 6 shows an example of two RBCs trajectories flowing in region  $R_{A500}$  and  $R_{B500}$ , in a parent microchannel with a width of 500  $\mu\text{m}$ , as well as the functions that have revealed a better approximation to the RBCs trajectories. Function  $g_1$  was not displayed mainly because it was the worst approximation solution to the cells trajectories. Overall, the numerical results suggest that the trigonometric function ( $g_3$ ) is the one that better resembles the RBCs trajectories and consequently the CFL boundaries, since for the majority of the cases studied the minimum value was obtained for this function. The trigonometric function ( $g_3$ ) may be due to oscillations caused by collisions between neighbourhood cells flowing around the RBCs core. The only exception was verified in the regions  $R_{A500}$ ,  $R_{A1000}$  and  $R_{B300}$ , wherein these regions the best fit was obtained with the function . Additionally, these results also show that the CFL boundary is size independent and its flow behaviour is not affected by complex geometries such bifurcations and confluences.

## Conclusions and Future Directions

In this study, we present a method to measure individual RBCs trajectories flowing around the CFL region. These cells trajectories are believed to closely resemble the CFL boundary and they were fitted using three different functions. A genetic algorithm was used to solve the constrained optimization problem and the best fit was obtained by using the function ( $g_3$ ), i.e., a sum of trigonometric functions. As a future work, we will test other functions and examine a bigger variety of physiological fluids used *in vitro* blood studies.

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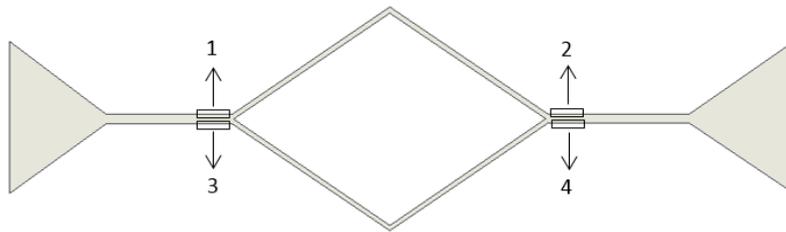
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## Illustrations

### Illustration 1

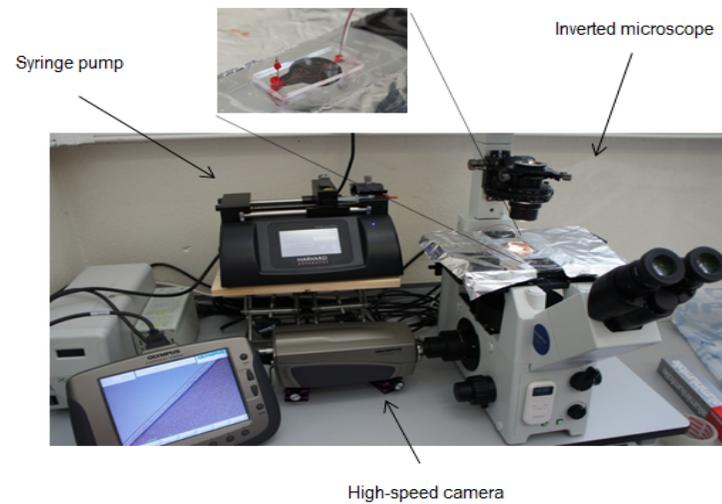
Schematic representation of the microchannel geometry and location of the sections where the images were collected and the CFL was measured.



- 1 – Region A ( $R_{A(\text{width})}$ );
- 2 – Region B ( $R_{B(\text{width})}$ );
- 3 – Region C ( $R_{C(\text{width})}$ );
- 4 – Region D ( $R_{D(\text{width})}$ );

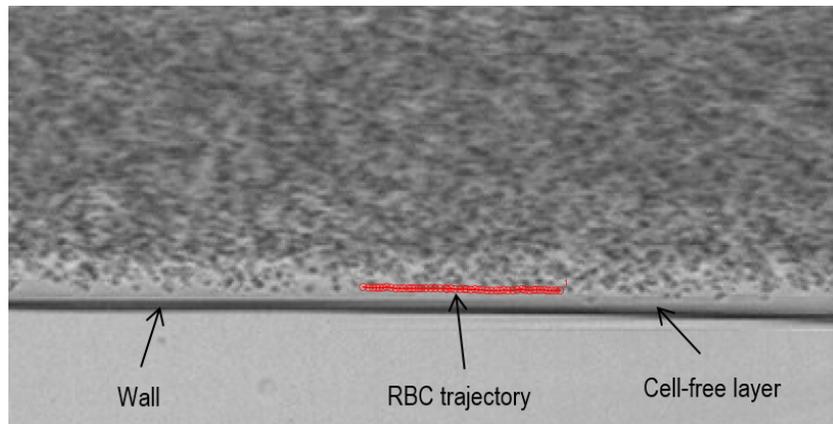
## Illustration 2

Experimental apparatus to control and visualize the flow in microchannels produced by xurography.



### Illustration 3

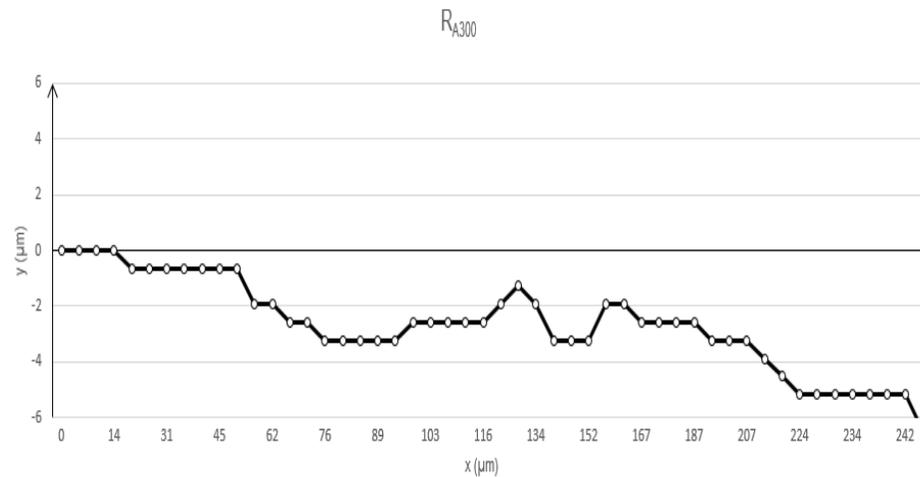
A trajectory of a RBC flowing around the boundary region between the CFL and RBCs core.



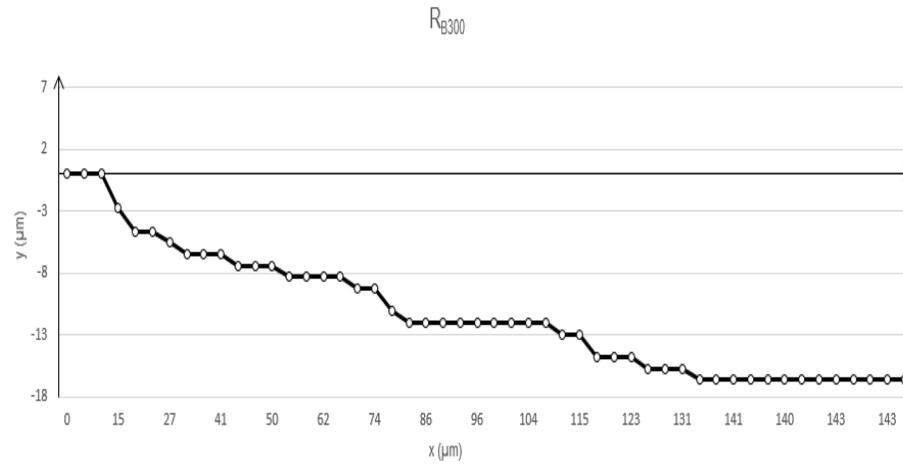
## Illustration 4

Trajectories of individual RBCs flowing around the CFL.

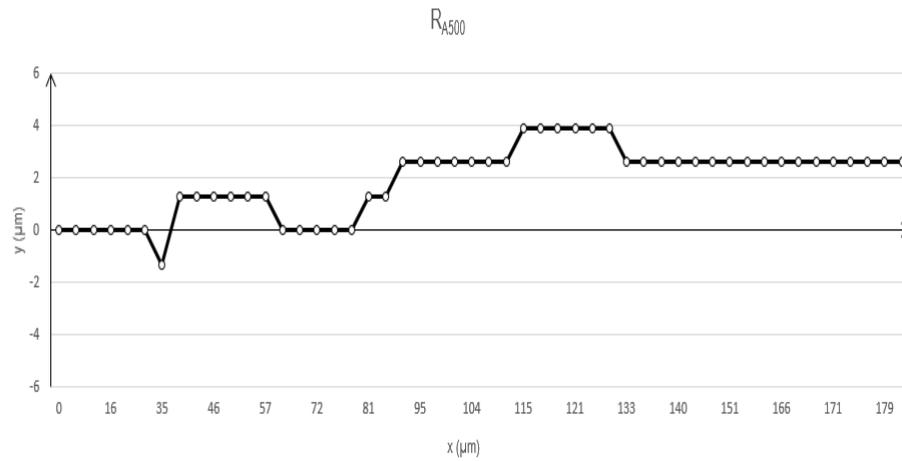
a) in region A at parent microchannel of 300  $\mu\text{m}$ ; b) in region B at parent microchannel of 300  $\mu\text{m}$ ; c) in region A at parent microchannel of 500  $\mu\text{m}$ ; d) in region B at parent microchannel of 500  $\mu\text{m}$ ; e) in region A at parent microchannel of 1000  $\mu\text{m}$ ; f) in region B at parent microchannel of 1000  $\mu\text{m}$ ; g) in region C at parent microchannel of 300  $\mu\text{m}$ ; h) in region D at parent microchannel of 300  $\mu\text{m}$ ; i) in region C at parent microchannel of 500  $\mu\text{m}$ ; j) in region D at parent microchannel of 500  $\mu\text{m}$ ; k) in region C at parent microchannel of 1000  $\mu\text{m}$ ; l) in region D at parent microchannel of 1000  $\mu\text{m}$ .



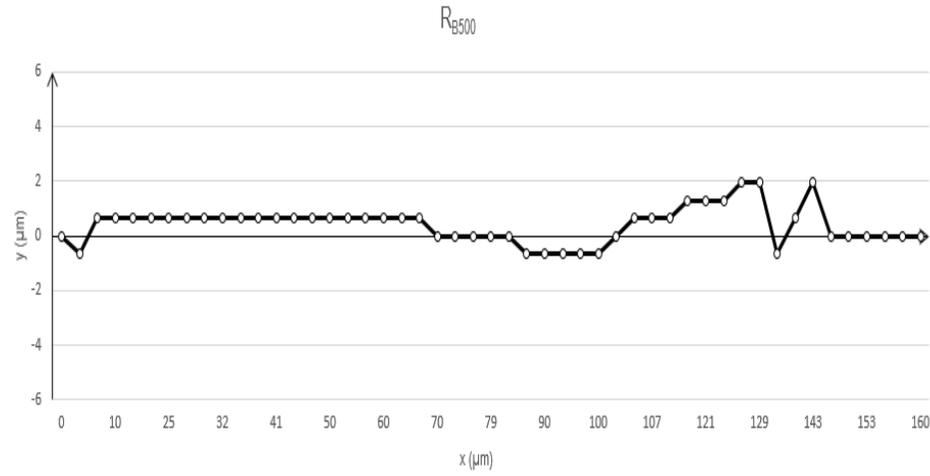
a)



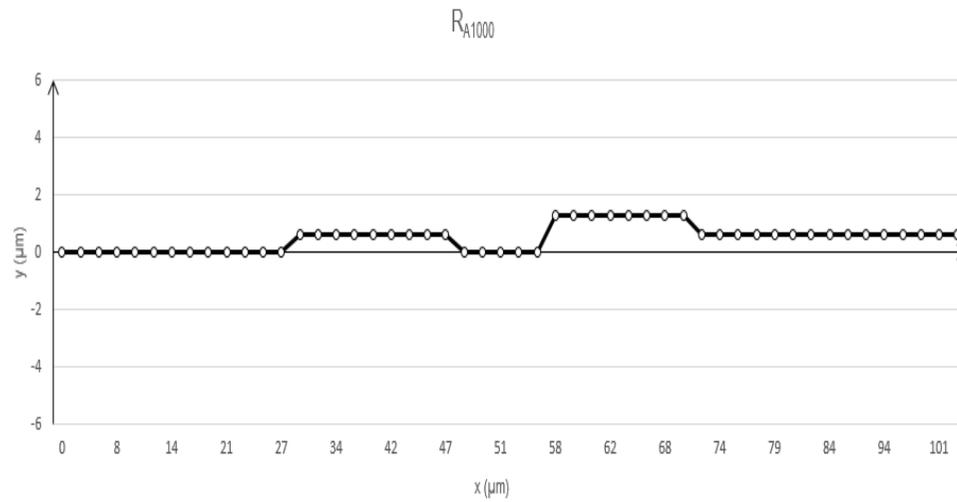
b)



c)



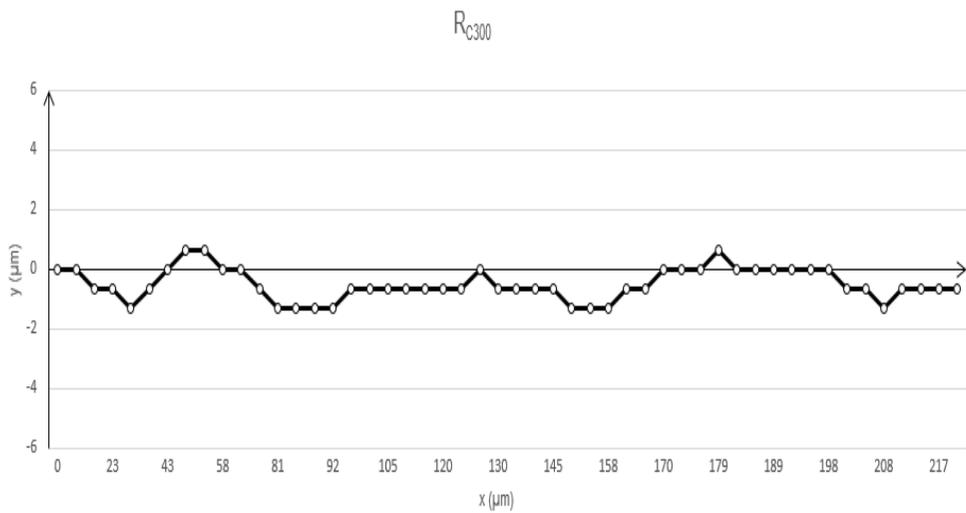
d)



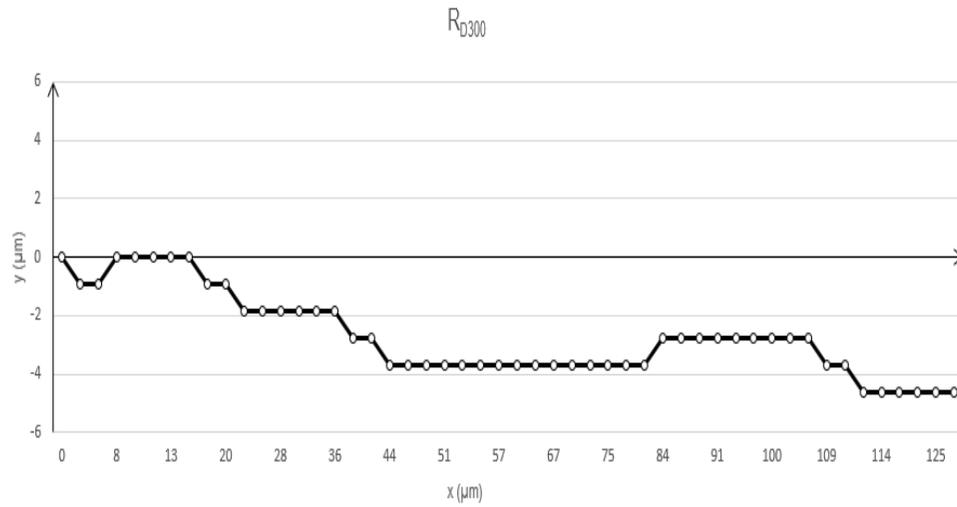
e)



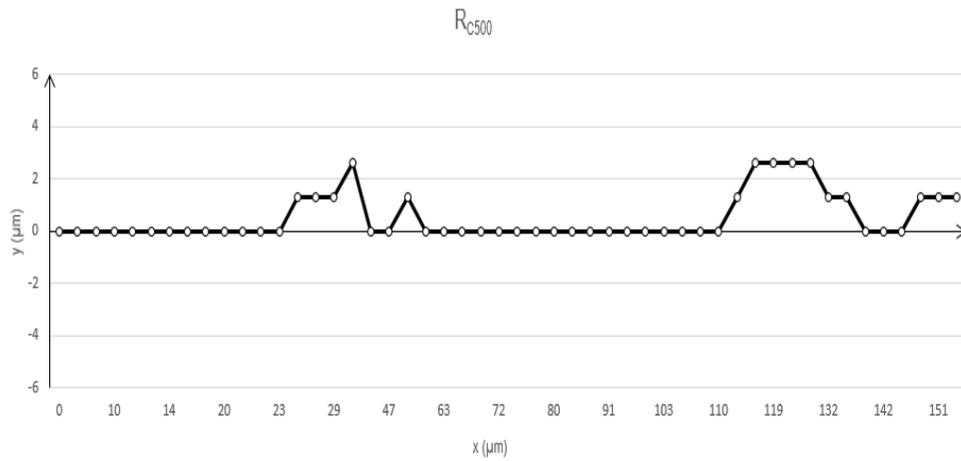
f)



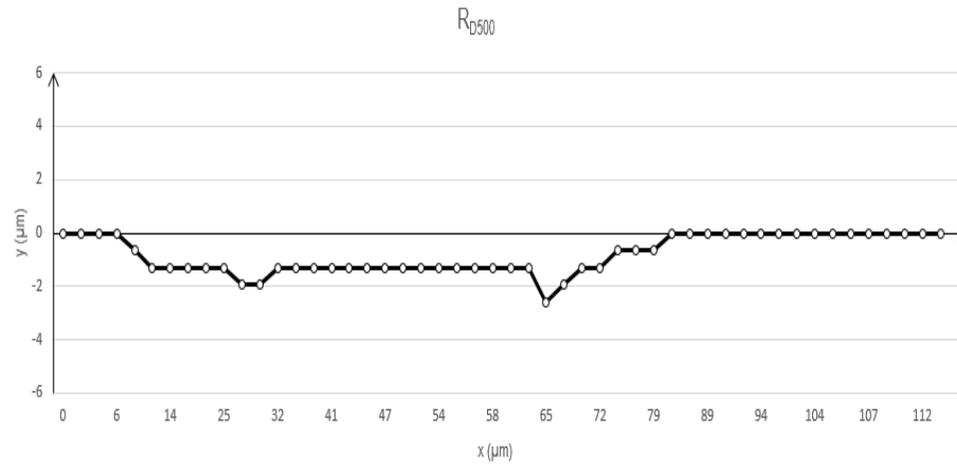
g)



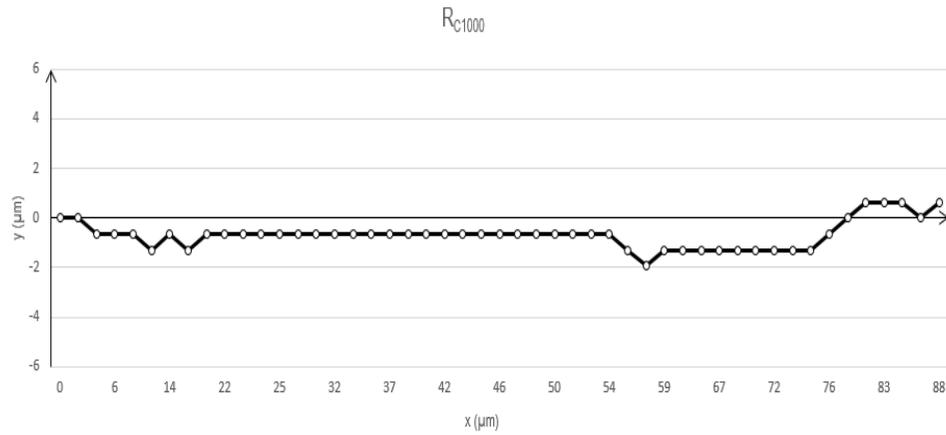
h)



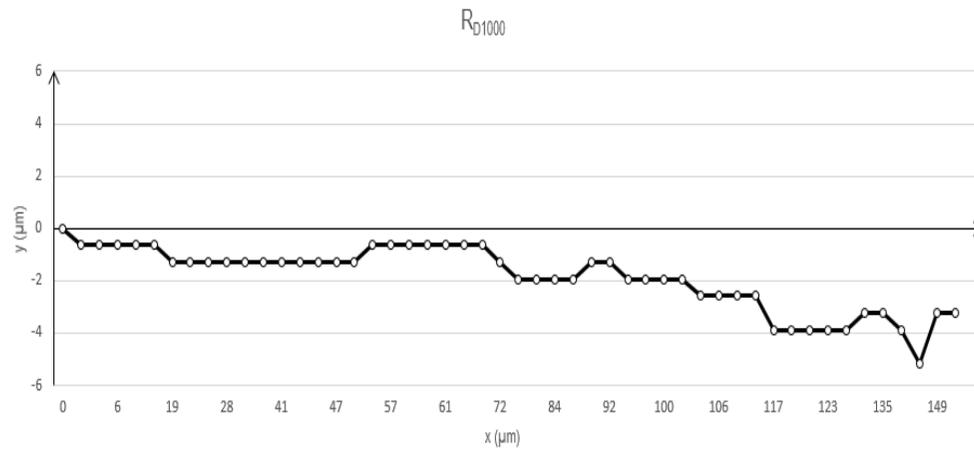
i)



j)



k)



l)

## Illustration 5

To obtain the numerical data a nonlinear least squares theory was used. In each region R<sub>Aw</sub>, R<sub>Bw</sub>, R<sub>Cw</sub>, and R<sub>Dw</sub> for  $w = 300, 500$  and  $1000$ , we have applied the nonlinear optimization problem defined as:

$$\min f(y) \equiv \sum_{k=1}^{N_R} (M_k - g_h(y, x_k))^2 \quad (1)$$

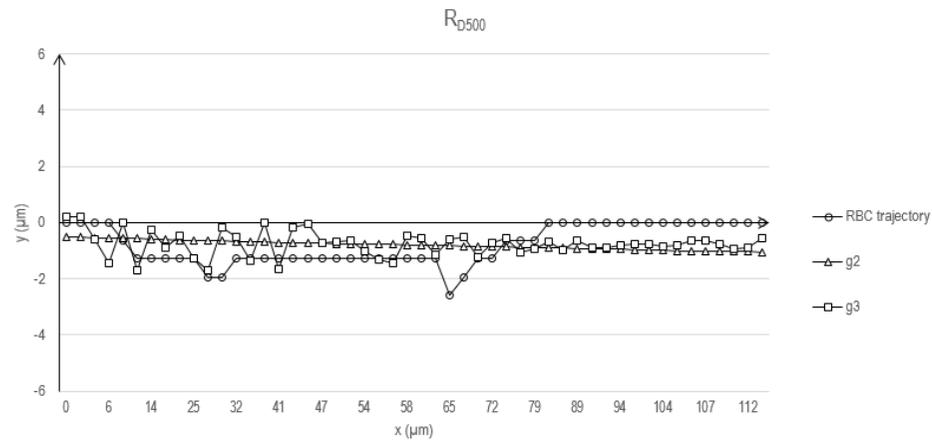
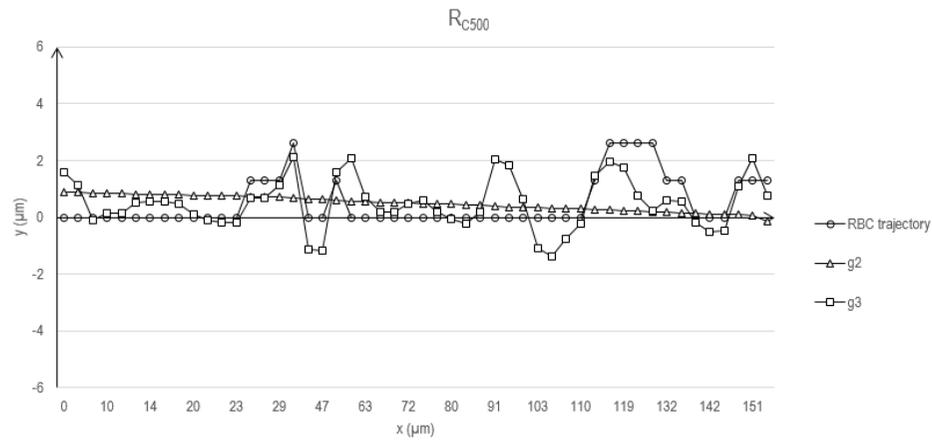
$$\text{s.t } g_h(y, x_k) \geq 0 \quad \forall k = 1, \dots, N_R$$

where  $(, )$ , for  $k = 1, \dots, N_R$  are the CFL measurement of region  $R$  (defined as R<sub>Aw</sub>, R<sub>Bw</sub>, R<sub>Cw</sub>, and R<sub>Dw</sub> for  $w = 300, 500$  and  $1000$ ). The function  $g_h$ , for  $h = 1, \dots, 3$ , are defined as follows:

$$\begin{aligned} g_1(y, x) &= y_1 x^2 + y_2 x + y_3, \\ g_2(y, x) &= y_1 x + y_2, \\ g_3(y, x) &= \sin(y_1 x) + \cos(y_2 x) + y_3. \end{aligned} \quad (2)$$

### Illustration 6

RBCs trajectories flowing in region RA500 and RB500, in a parent microchannel with a width of 500 &micro;m, as well as the functions that have showed a better approximation.



## Illustration 7

Numerical results obtained using a genetic algorithm.

Region	Function	Average	Minimun
RA300	91	4,90E+05	52,18
	92	7,54E+01	31,90
	<b>93</b>	<b>7,39E+01</b>	<b>26,89</b>
RA500	91	1,29E+05	59,82
	<b>92</b>	<b>6,24E+01</b>	<b>38,76</b>
	93	7,00E+01	45,07
RA1000	91	2,00E+04	20,98
	<b>92</b>	<b>1,23E+01</b>	<b>6,46</b>
	93	2,09E+01	8,89
RB300	91	8,94E+04	97,17
	<b>92</b>	<b>6,93E+01</b>	<b>30,42</b>
	93	7,86E+02	621,43
RB500	91	1,37E+05	54,71
	92	3,99E+01	20,63
	<b>93</b>	<b>3,25E+01</b>	<b>19,64</b>
RB1000	91	1,58E+05	50,98
	92	2,73E+01	14,33
	<b>93</b>	<b>3,24E+01</b>	<b>11,09</b>

<b>RC300</b>	91	2,89E+05	42,35
	92	4,88E+01	13,86
	<b>93</b>	<b>2,45E+01</b>	<b>10,50</b>
<b>RC500</b>	91	7,30E+04	57,04
	92	4,66E+01	32,60
	<b>93</b>	<b>3,93E+01</b>	<b>26,63</b>
<b>RC1000</b>	91	1,37E+04	11,36
	92	2,16E+01	14,82
	<b>93</b>	<b>2,06E+01</b>	<b>6,42</b>
<b>RD300</b>	91	4,20E+04	31,76
	92	5,42E+01	35,33
	<b>93</b>	<b>5,23E+01</b>	<b>14,36</b>
<b>RD500</b>	91	2,87E+04	13,32
	92	2,96E+01	19,96
	<b>93</b>	<b>2,18E+01</b>	<b>6,78</b>
<b>RD1000</b>	91	6,92E+04	58,85
	92	4,32E+01	18,71
	<b>93</b>	<b>3,50E+01</b>	<b>13,60</b>

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